

Light Reflectors and Optical Resonators

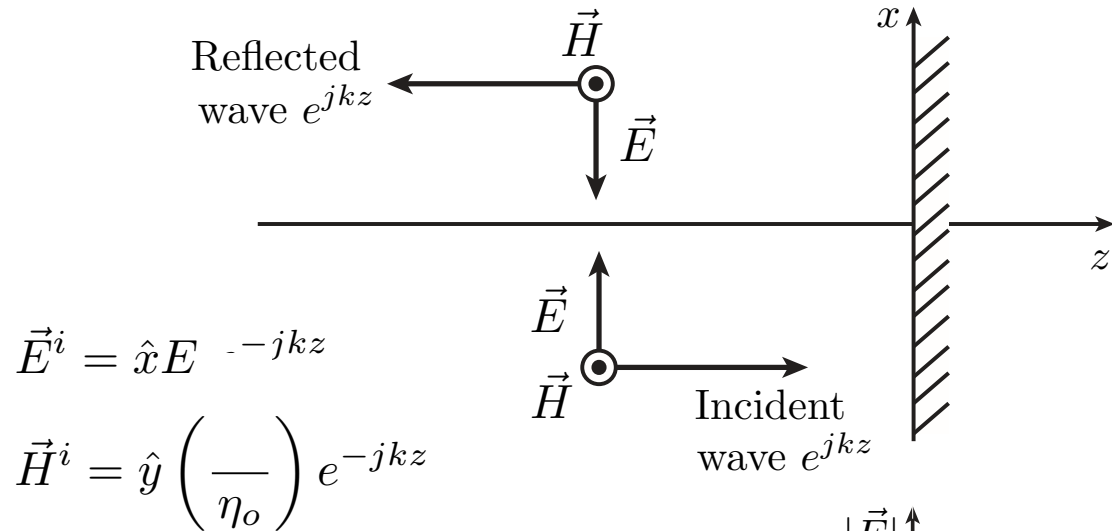
Outline

Review of Wave Reflection
Reflection and Interference
Fiber for Telecommunications
Optical Resonators

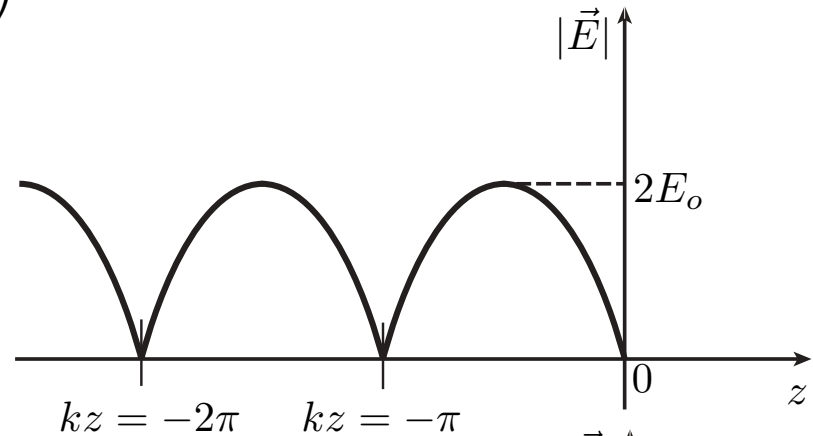
Reflection of a Normally Incident EM Wave from a Perfect Conductor



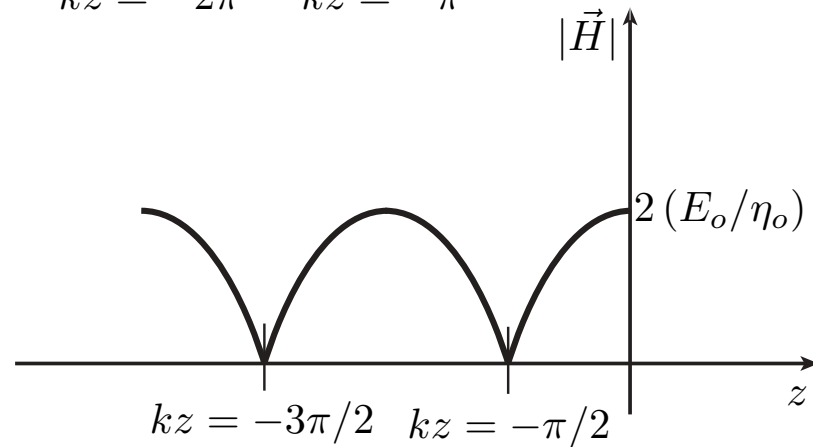
Image by Theogeo <http://www.flickr.com/photos/theogeo/1102816166/> on flickr



Standing wave pattern of the E-field



Standing wave pattern of the H-field



Reflection & Transmission of EM Waves at Boundaries

$$\begin{aligned}\vec{E}_1 &= \vec{E}_i + \vec{E}_r \\ &= \hat{x} \left(E_o^i e^{-jk_1 z} + E_o^r e^{+jk_1 z} \right)\end{aligned}$$

$$\begin{aligned}\vec{E}_2 &= \vec{E}_t \\ &= \hat{x} E_o^t e^{-jk_2 z}\end{aligned}$$

Medium 1

Medium 2

$$\begin{aligned}\vec{H}_1 &= \vec{H}_i + \vec{H}_r \\ &= \hat{y} \left(\frac{E_o^i}{\eta_1} e^{-jk_1 z} - \frac{E_o^r}{\eta_1} e^{+jk_1 z} \right)\end{aligned}$$

$$\begin{aligned}\vec{H}_2 &= \vec{H}_t \\ &= \hat{y} \frac{E_o^t}{\eta_2} e^{-jk_2 z}\end{aligned}$$

$$\overline{E}_1(z=0) = \overline{E}_2(z=0)$$

$$\overline{H}_1(z=0) = \overline{H}_2(z=0)$$

Reflection of EM Waves at Boundaries

$$\vec{E}_1(z = 0) = \vec{E}_2(z = 0)$$

$$E_o^i + E_o^r = E_o^t$$

$$\vec{H}_1(z = 0) = \vec{H}_2(z = 0)$$

$$\frac{E_o^i}{\eta_1} - \frac{E_o^r}{\eta_1} = \frac{E_o^t}{\eta_2} \quad \eta = \sqrt{\frac{\mu}{\epsilon}}$$

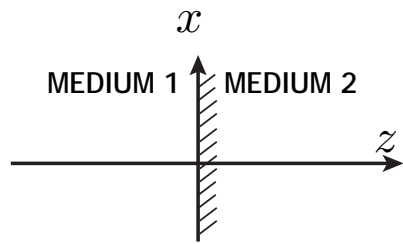
$$r = \frac{E_o^r}{E_o^i} = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$$

REFLECTION COEFFICIENT

(note that sign of r depends on the relative values of η_2 and η_1)

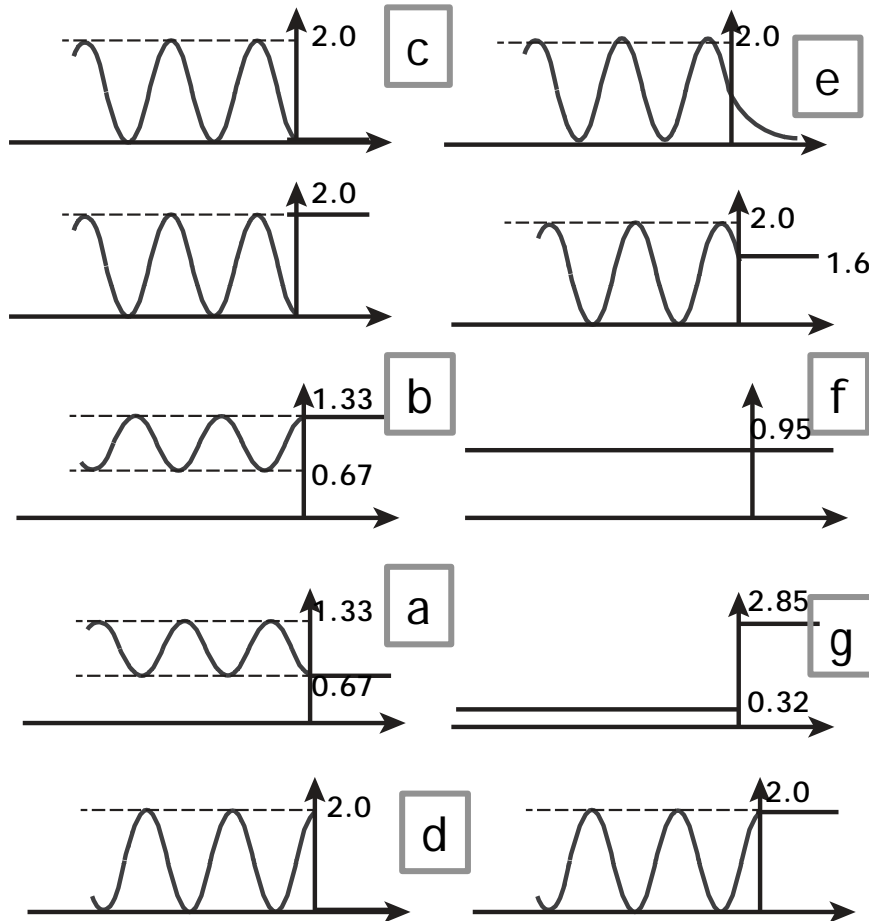
$$t = \frac{E_o^t}{E_o^i} = \frac{2\eta_2}{\eta_2 + \eta_1}$$

TRANSMISSION COEFFICIENT



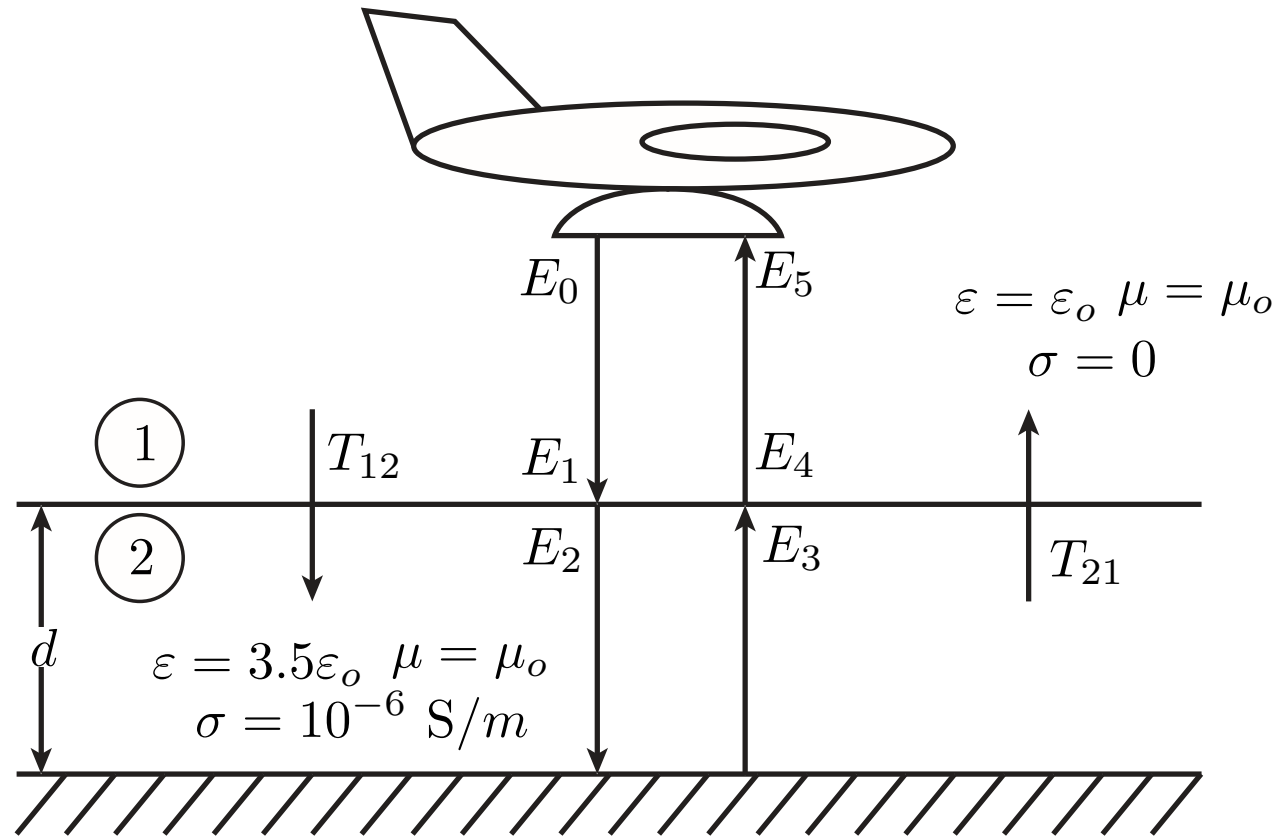
Examples of Light Reflection

The image below indicates the standing wave patterns ($|E_i + E_r|$) resulting when an incident wave in medium 1 with amplitude equal to 1 V/m is incident on an interface. Label the graphs (a)-(g) to match them with the description detailed below.



- Plot of $|E_{y,total}|$ with medium 1 being air, medium 2, $n_2 = 2$. Normal incidence.
- Plot of $|E_{y,total}|$ with medium 1 having $n_1 = 2$, medium 2 being air. Normal incidence.
- Plot of $|E_{y,total}|$ with medium 1 being air, medium 2 being a perfect conductor
- Plot of $|H_{y,total}|$ with medium 1 being air, medium 2 being a perfect conductor
- Plot of $|E_{y,total}|$ with medium 1 having $n_1 = 2$, medium 2 being air. Angle of incidence greater than critical angle.
- Plot of $|E_{y,total}|$ with angle of incidence equal to the Brewster angle.
- Plot of $|E_{y,total}|$ with angle of incidence equal to the Brewster angle. Medium 2 is air.

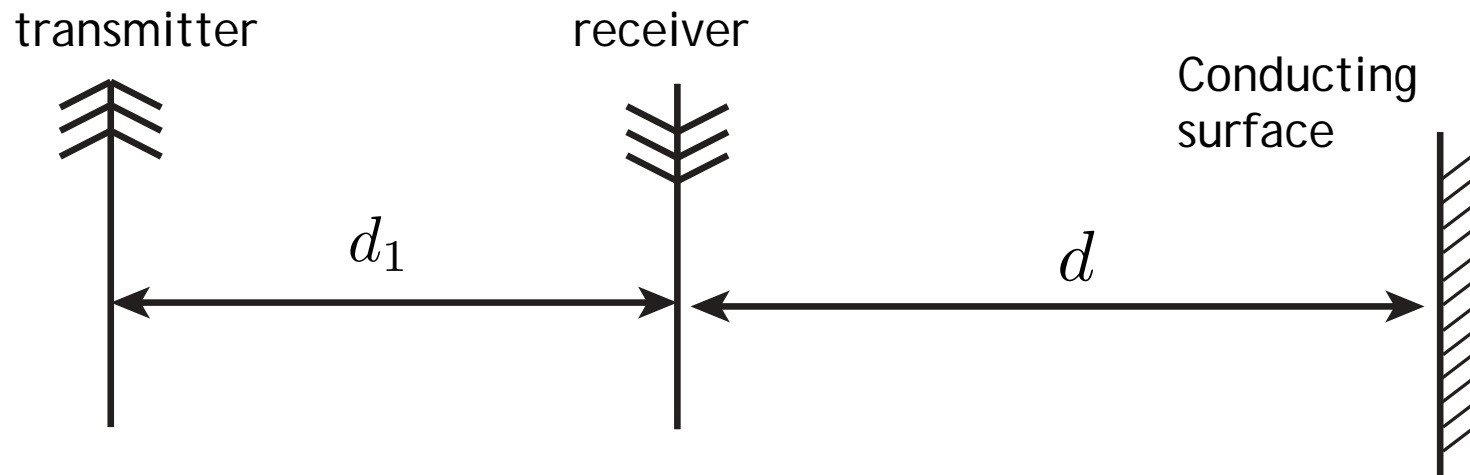
Remote Sensing of the Environment ... using radar



EXAMPLE: MEASUREMENT OF THICKNESS OF POLAR ICE CAPS

Reflectometry

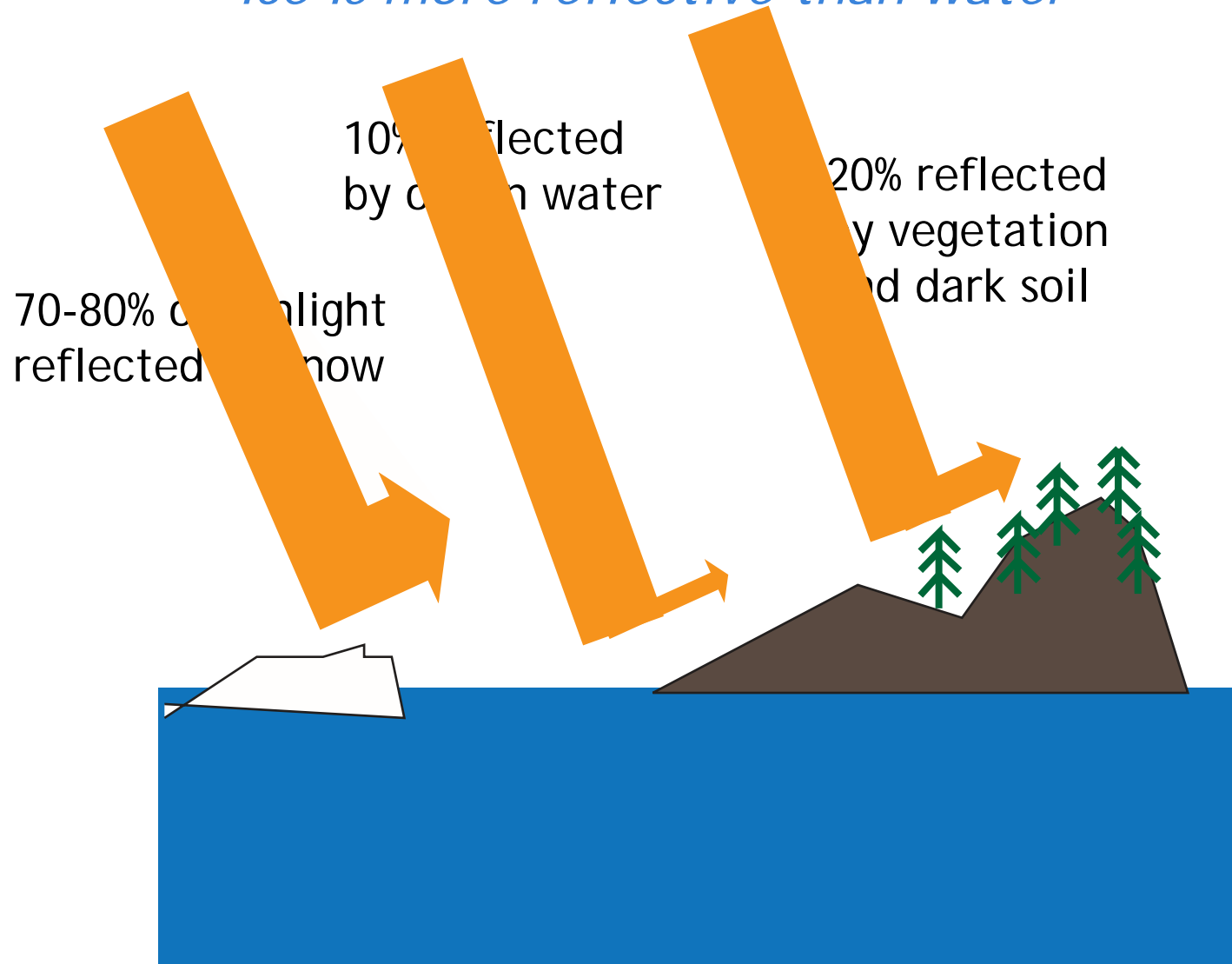
... measurement of distance to a target by identifying the nodes in the standing wave pattern





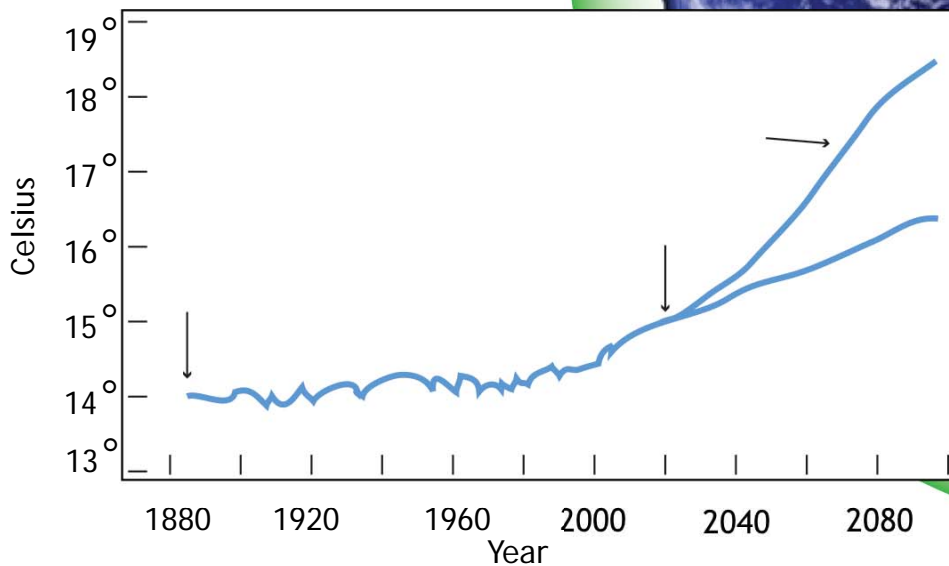
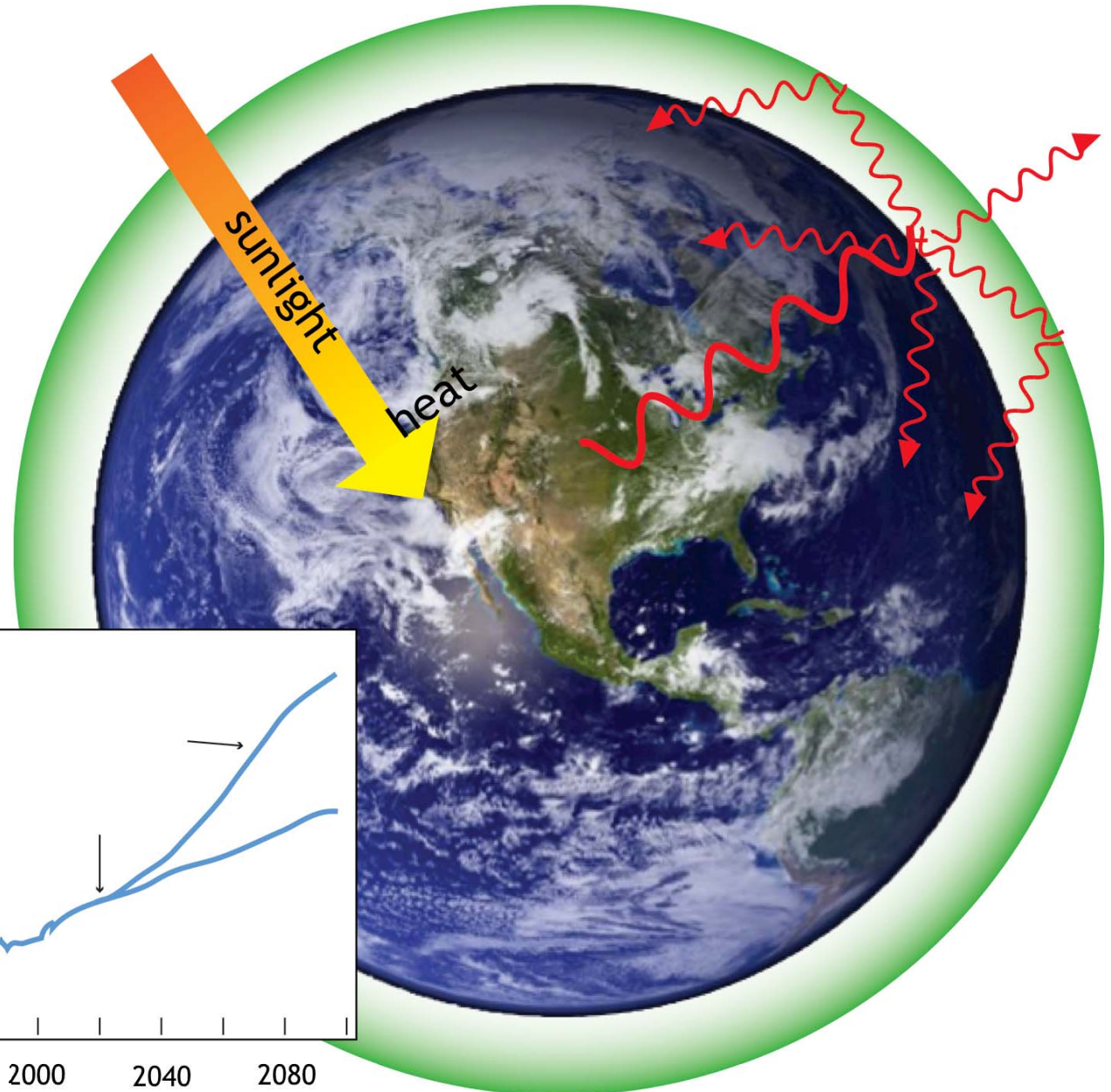
Today's Culture Moment

Ice is more reflective than water



The Greenhouse Effect

Sunlight is reradiated as heat and trapped by greenhouse gasses such as carbon dioxide. Too much carbon dioxide, however, causes the planet to heat up more than usual.



Deploy Aluminum Rafts over Dead Ocean Areas ?

Net excess energy input into planet Earth 1.6 W/m^2 .

Illuminance on ground level is $\sim 1000 \text{ W/m}^2$

→ We need to reflect $1.6/1000$ of energy back to Balance the Energy IN/OUT

Oceans are 90% absorptive (10% reflective)

Aluminum is 88% reflective on the shiny side and 80% reflective on the dull side.
(Frosted silica might also be able to be used as a reflector)

How much of ocean area do we need to cover
with 80% reflective sheets of aluminum to balance the energy IN/OUT ?
 $(1.6/1000) / (80\% - 10\%) = 0.23\%$ (of the Earth's surface area)

Earth surface area = 5100 million km^2

We need to cover = 1.2 million km^2

→ equivalent to ~ 100 years
of today's Aluminum production
(assuming $50 \mu\text{m}$ thick Al foil)

Dead ocean zones = 0.24 million km^2

Ice fields:

North Pole = 9 to 12 million km^2

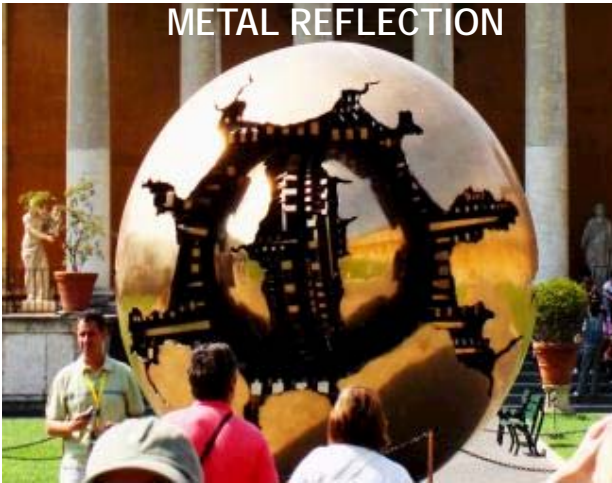
Greenland ice sheet = 1.7 million km^2

South Pole = 14 million km^2



Image is in the public domain

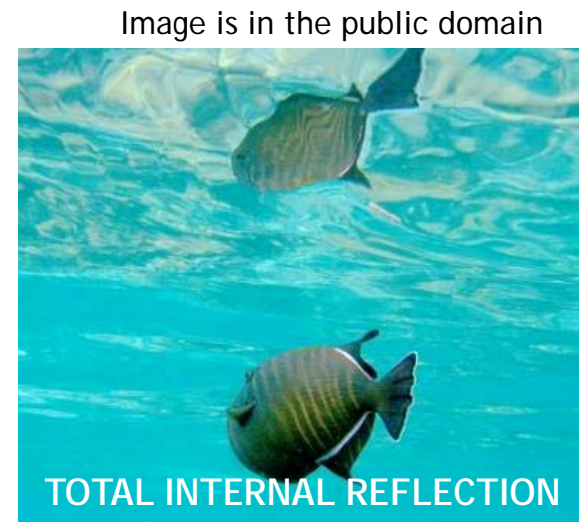
Three Ways to Make a Mirror



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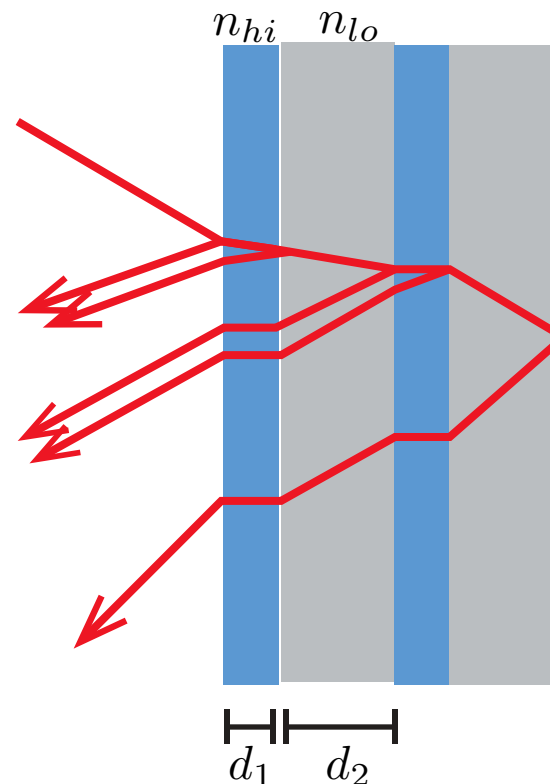
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File:Dielectric_laser_mirror_from_a_dye_laser.JPG](http://en.wikipedia.org/wiki/File:Dielectric_laser_mirror_from_a_dye_laser.JPG)



Dielectric Mirrors

... can be >99% reflective

Simple dielectric mirrors consist of stacked of layers of high and low refractive index. The layers are chosen such the path-length differences of reflections from low to high index layers are integer multiples of wavelengths. Similarly, reflections from low-index layers have path length difference of half a wavelength, but add constructively because of 180 degree phase shift from the reflection. For normal incidence, these optimized thicknesses are a quarter of a wavelength



$$R = \left(\frac{1 - b}{1 + b} \right)^2 \quad b = \prod_{i=0}^N \left[\frac{n_{LO}}{n_{HI}} \right] \quad \begin{aligned} d_1 &= \lambda / (4n_{hi}) \\ d_2 &= \lambda / (4n_{lo}) \end{aligned}$$

Thin layers with a high refractive index n_{HI} are interleaved with thicker layers with a lower refractive index n_{LO} . The path lengths l_A and l_B differ by exactly one wavelength, which leads to constructive interference.

Source: wikipedia.com

Opals

... are an example of dielectric mirrors

Colors with $\lambda = 2d \sin(\alpha)$ have constructive interference

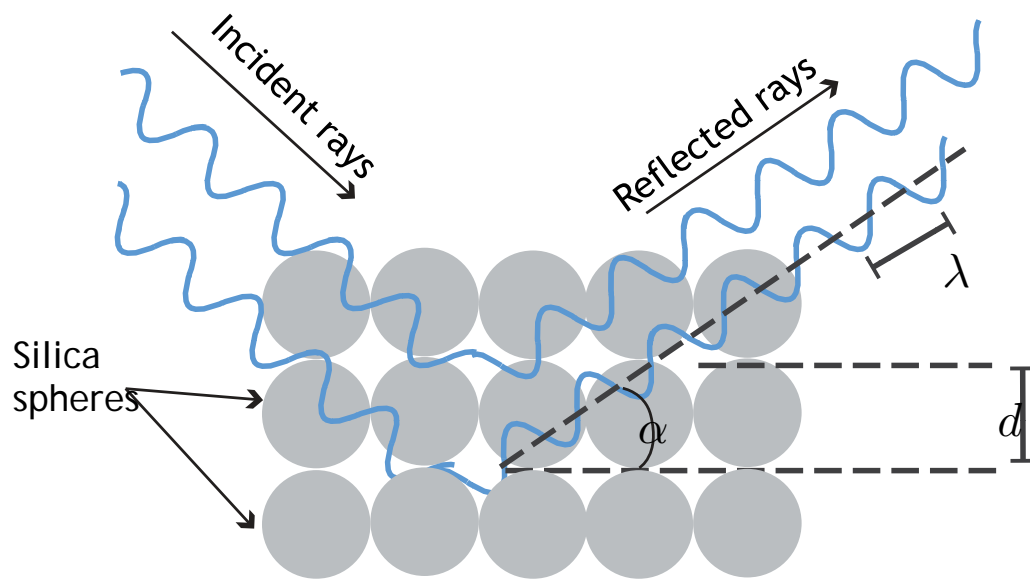
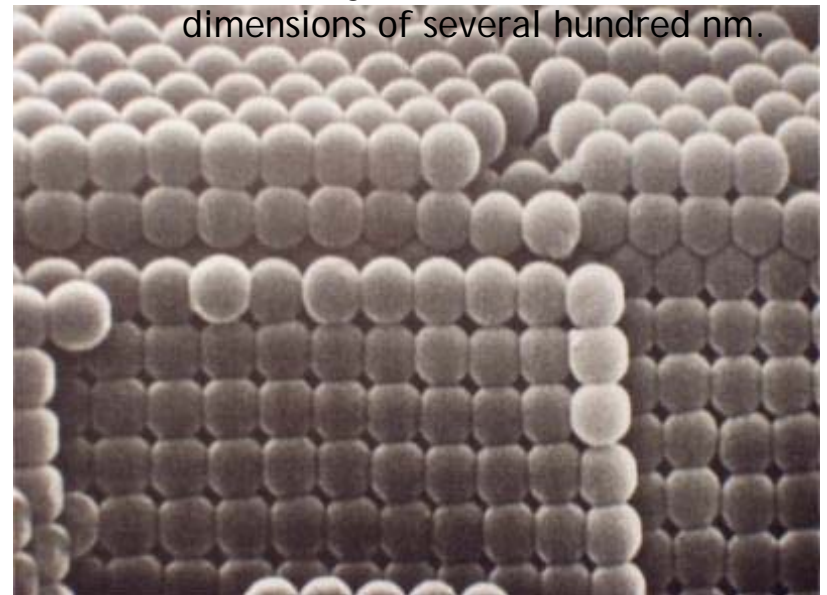


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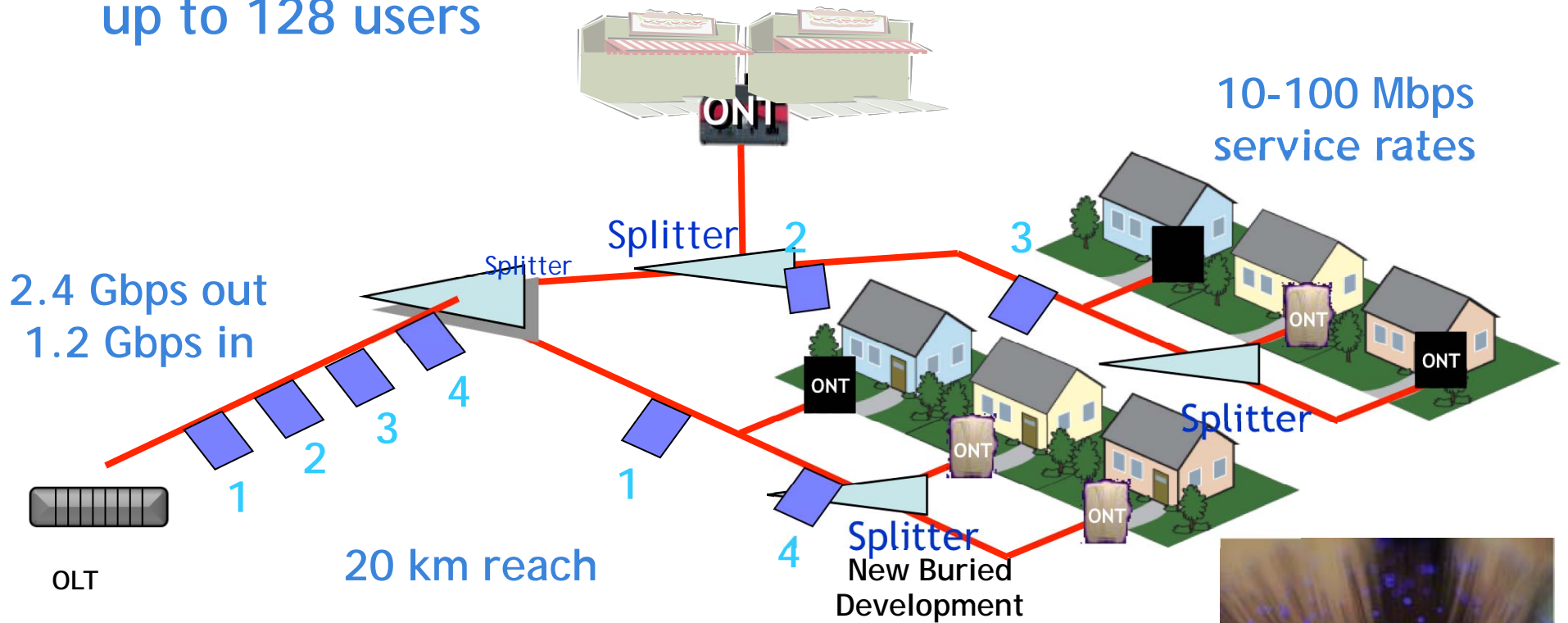
Precious opal consists of spheres of silica of fairly regular size, packed into close-packed planes that are stacked together with characteristic dimensions of several hundred nm.



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Fiber to the Home

2.4 Gbps shared by up to 128 users



Time Division Multiplexing

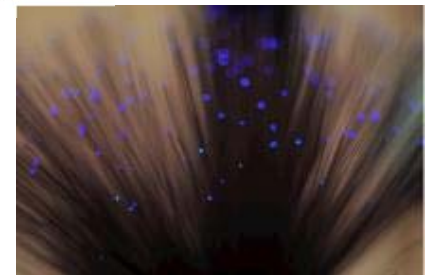
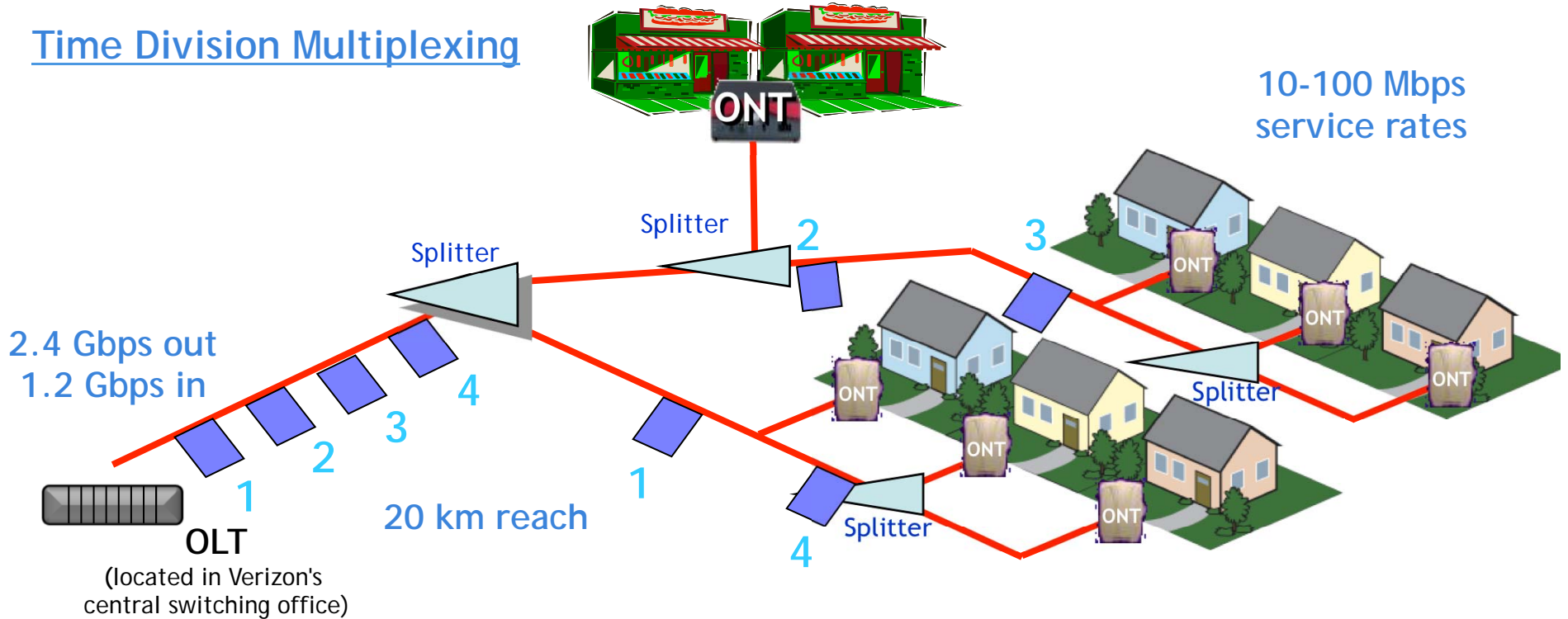


Image by Dan Tentler <http://www.flickr.com/photos/vissago/4634464205/> on flickr

Fiber to the Home

Time Division Multiplexing



An ONT (Optical Network Terminal) is a media converter that is installed by Verizon either outside or inside your premises, during FiOS installation. The ONT converts fiber-optic light signals to copper/electric signals. Three wavelengths of light are used between the ONT and the OLT (Optical Line Terminal):

- $\lambda = 1310$ nm voice/data transmit
- $\lambda = 1490$ nm voice/data receive
- $\lambda = 1550$ nm video receive

Each ONT is capable of delivering:
Multiple POTS (plain old telephone service) lines, Internet data, Video

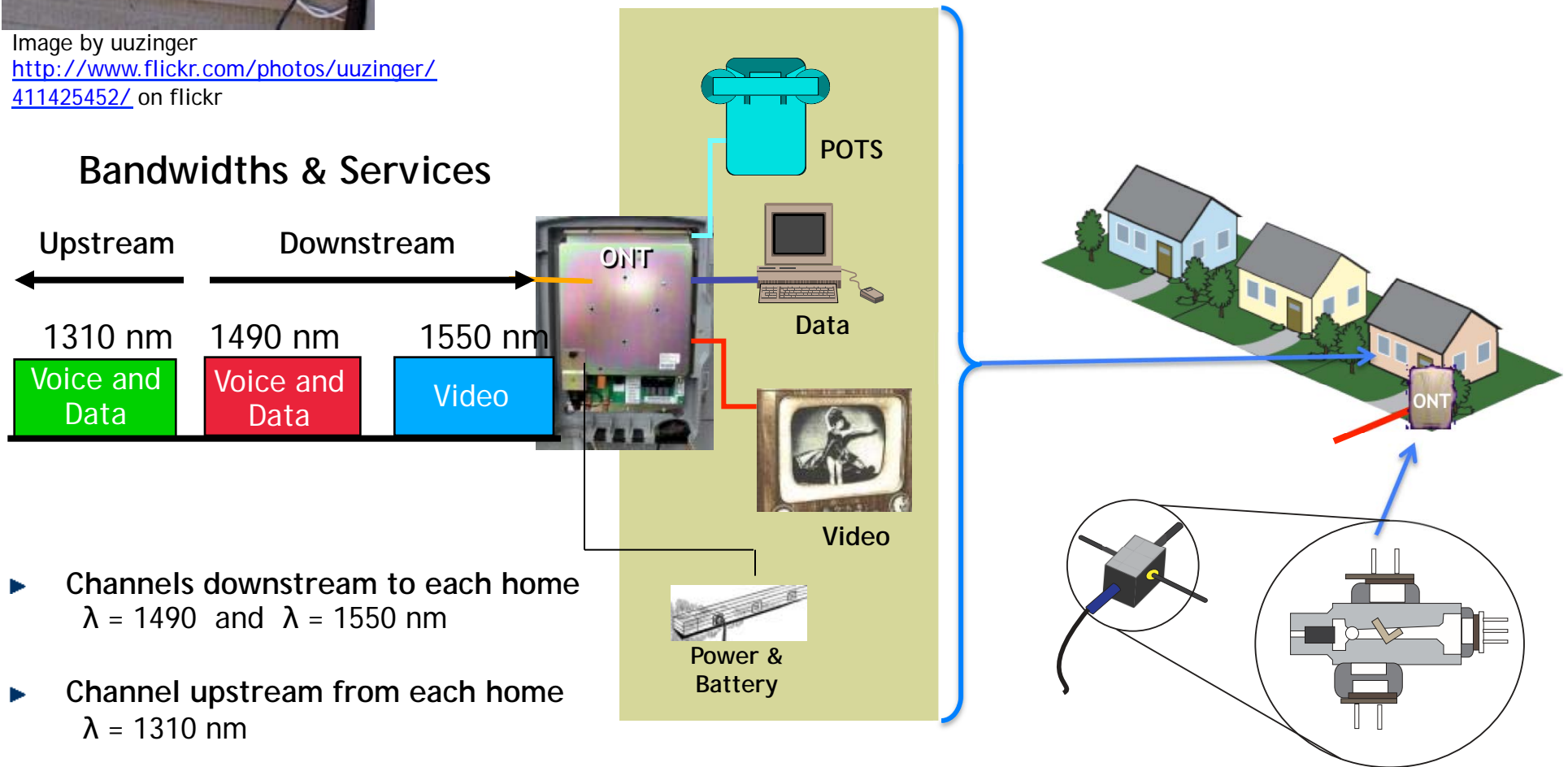
Fiber to the Home



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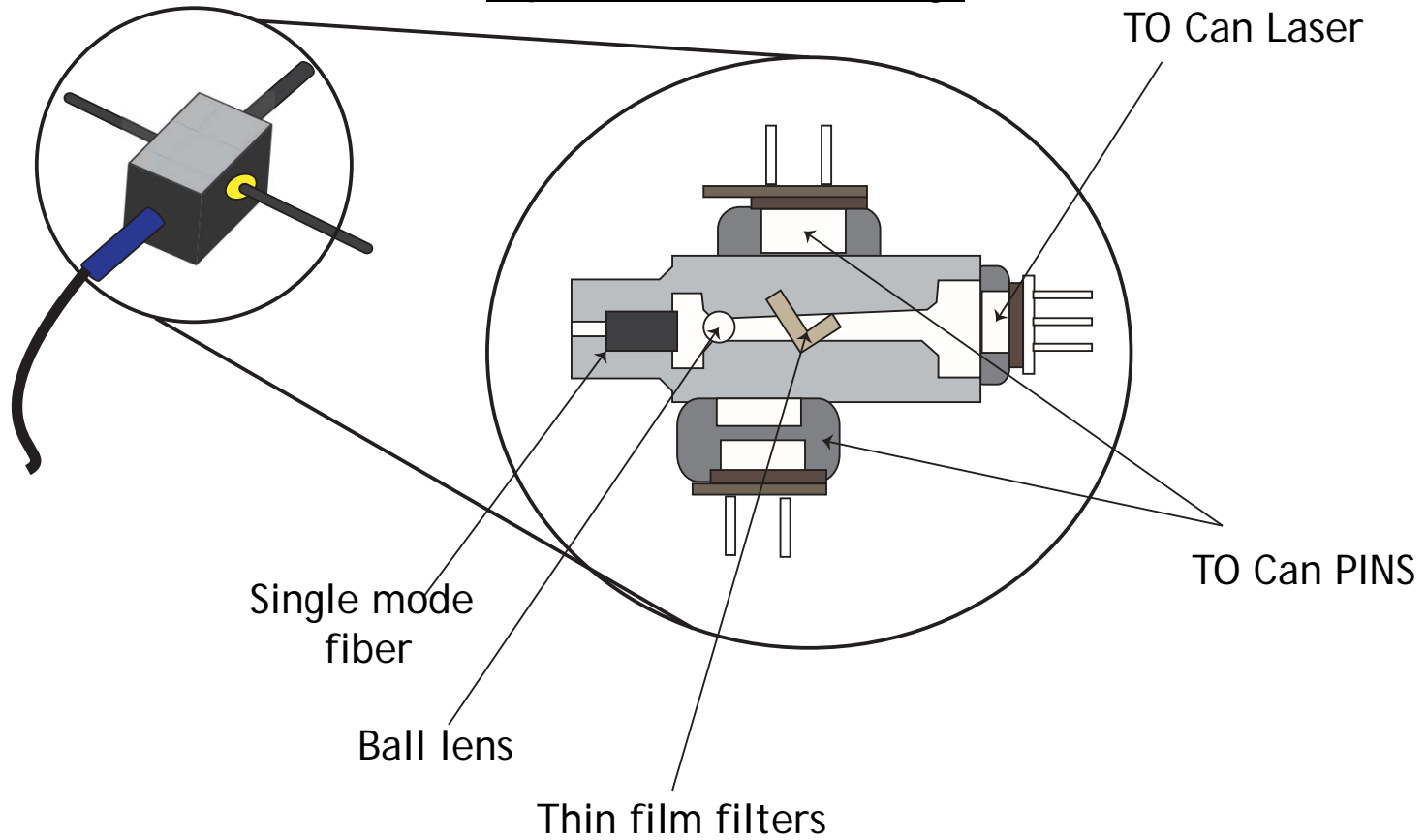
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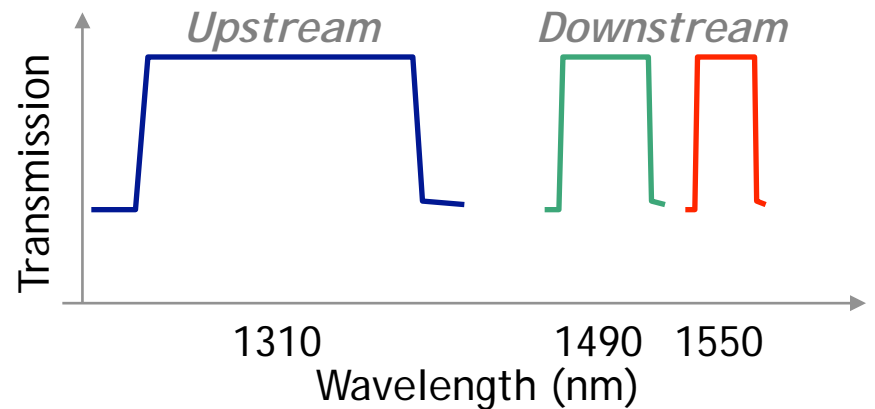
- ▶ Channels downstream to each home
 $\lambda = 1490$ and $\lambda = 1550$ nm
- ▶ Channel upstream from each home
 $\lambda = 1310$ nm

Image of ONT by Josh Bancroft
<http://www.flickr.com/photos/joshb/87167324/> on flickr

Optical Assembly



- ▶ Channels downstream to each home
 - ▶ $\lambda = 1490$ and $\lambda = 1550$ nm
- ▶ Channel upstream from each home
 - ▶ $\lambda = 1310$ nm



Separating Wavelengths

Dispersion

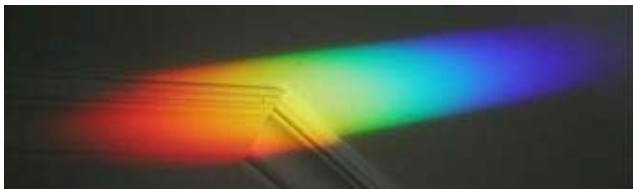


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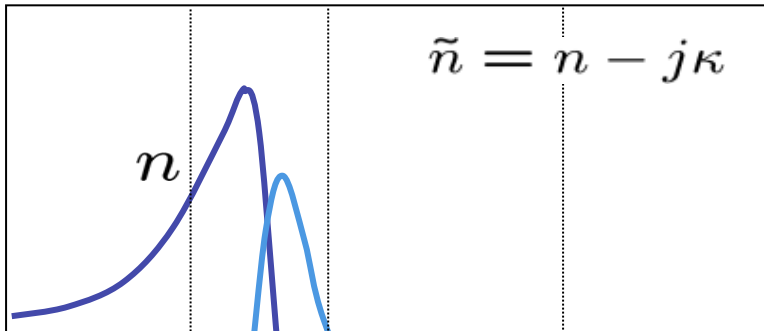
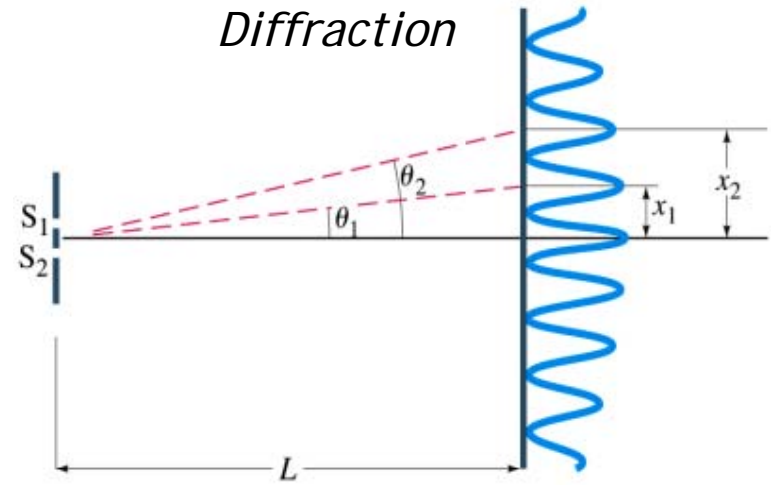


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Diffraction



Sunlight diffracted through a 20 μm slit

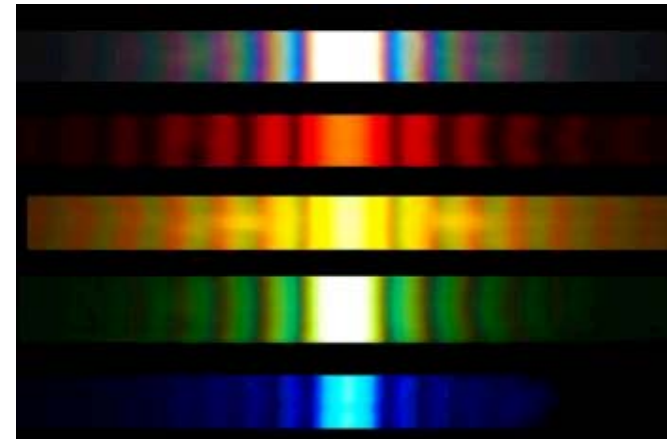
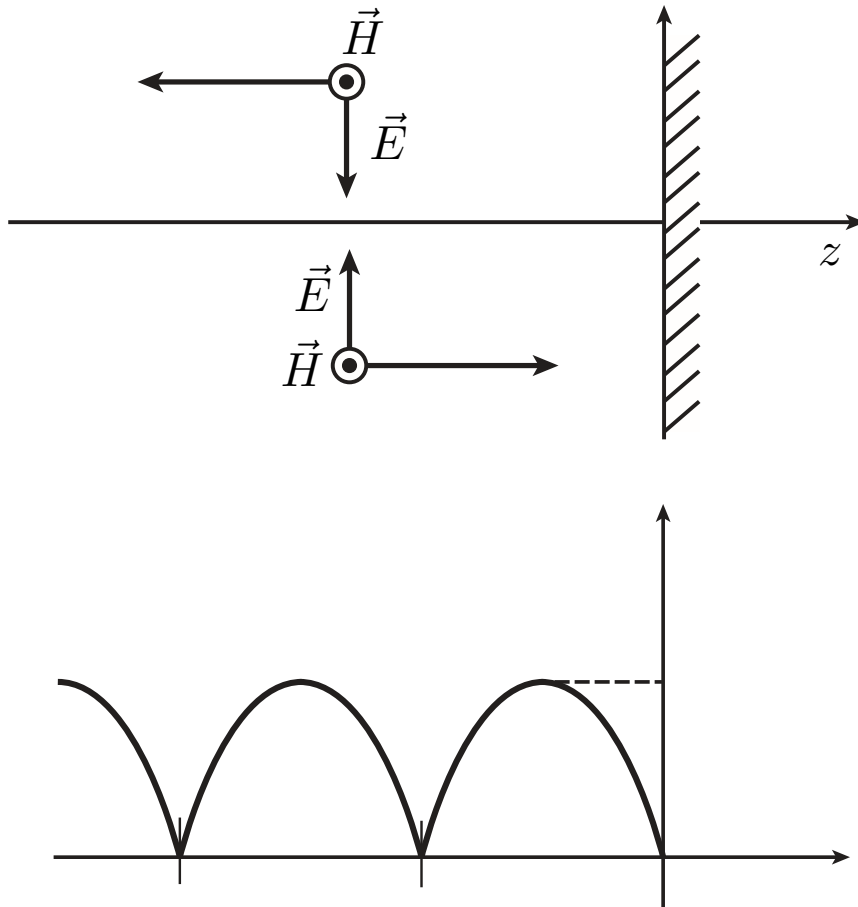


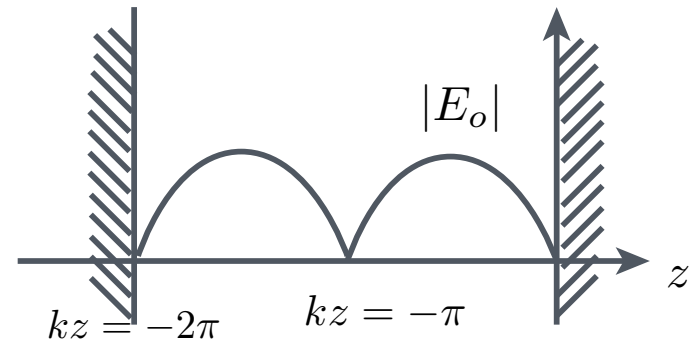
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Resonators

STANDING WAVE



RESONATORS

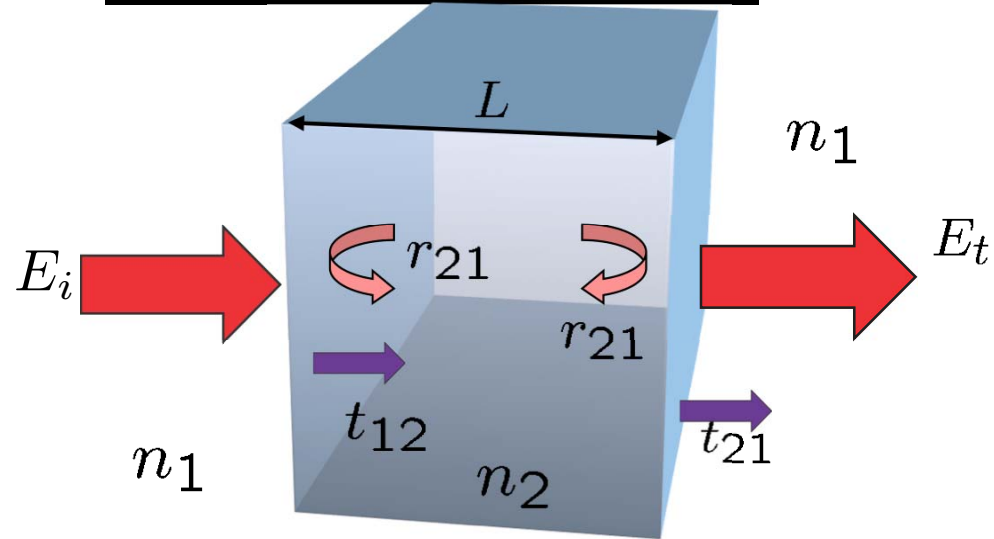


↑
Terminate the standing wave with a second wall to form a resonator



Image by Yoko Nekonomania <http://www.flickr.com/photos/nekonomania/4827035737/> on flickr

Thin Film Interference



$$t_{12} (r_{21})^3 t_{21} E_i e^{-j\beta_2 2L}$$

$$t_{12} r_{21} t_{21} E_i e^{-j\beta_2 2L}$$

$$r_{12} E_i$$

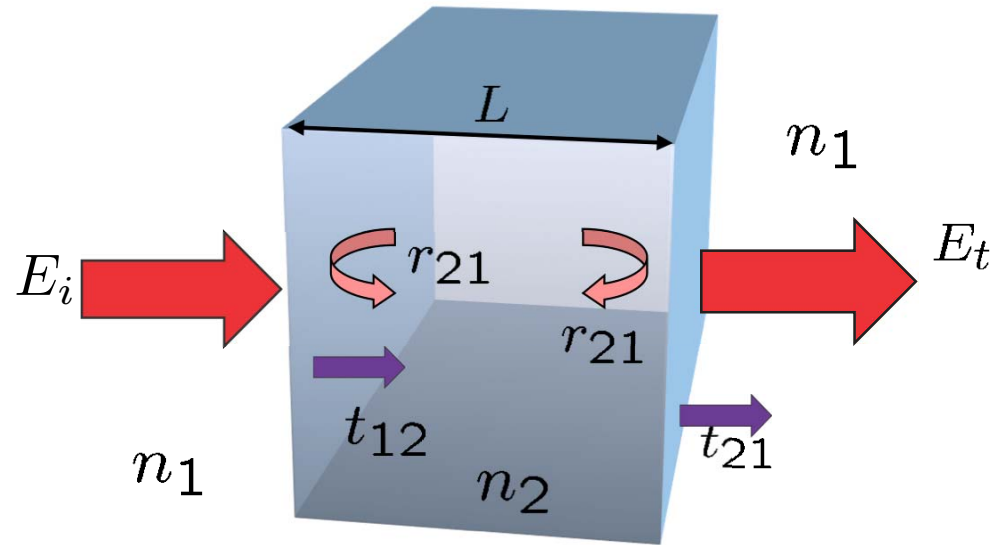
$$E_i$$

$$t_{12} E_i$$

$$t_{12} r_{21} r_{21} t_{21} E_i e^{-j\beta_2 2L}$$

$$t_{12} t_{21} E_i e^{-j\beta_2 2L}$$

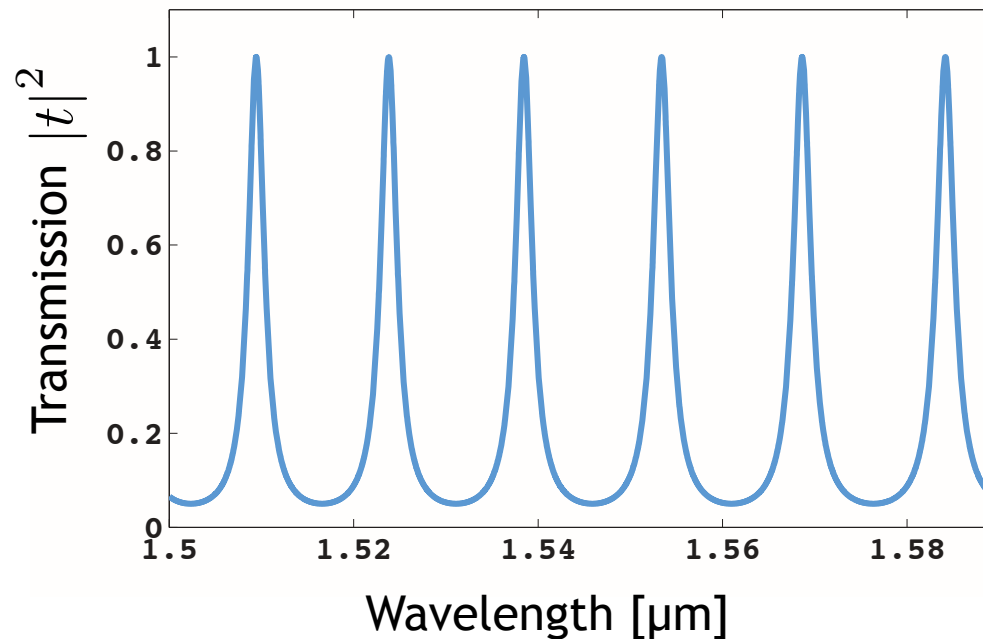
Optical Resonator



$$\begin{aligned}
 E_t &= [t_{12}t_{21}e^{-j\beta_2 L} + t_{12}e^{-j\beta_2 L}r_{21}e^{-j\beta_2 L}r_{21}e^{-j\beta_2 L}t_{21}\dots] E_i \\
 &= \left[t_{12}t_{21}e^{-j\beta L} \left(1 + r_{12}r_{21}e^{-2j\beta L} + (r_{12}r_{21}e^{-2j\beta L})^2 \dots \right) \right] E_i \\
 &= \frac{t_{12}t_{21}e^{-j\beta_2 L}}{1 - r_{12}r_{21}e^{-2j\beta L}} E_i
 \end{aligned}$$

Fabry-Perot Resonance

$$t = \frac{t_{12}t_{21}e^{-jkL}}{1 - r_{12}r_{21}e^{-2jkL}}$$



Fabry-Perot Resonance: $\max\{e^{-2jk_2L}\} = 1$ maximum transmission

$\min\{e^{-2jk_2L}\} = -1$ minimum transmission

Total Internal Reflection

Beyond the critical angle, θ_c , a ray within the higher index medium cannot escape at shallower angles

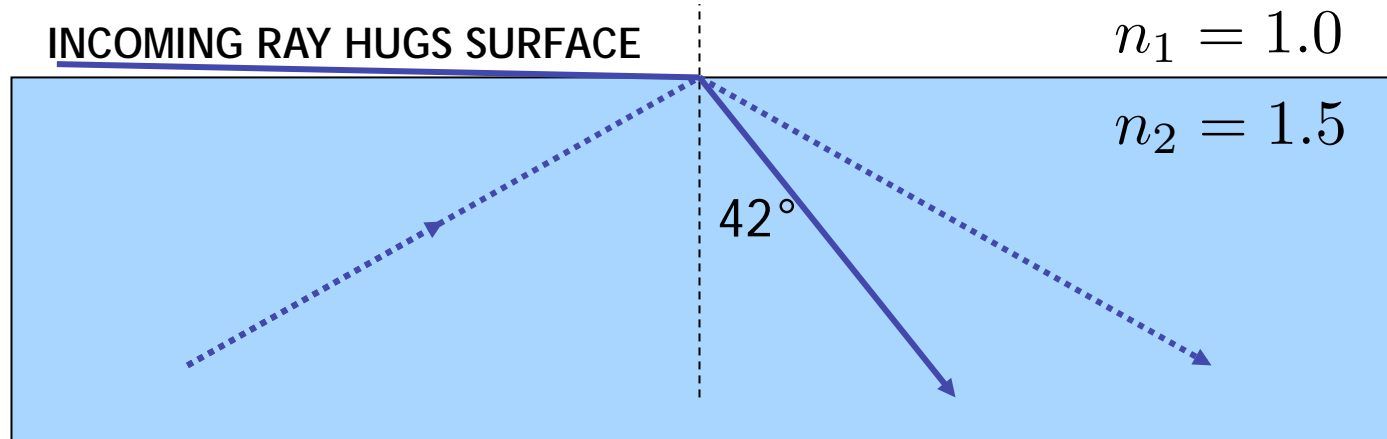
$$n_2 \sin \theta_2 = n_1 \sin \theta_1 \quad \theta_c = \sin^{-1}(n_1/n_2)$$

For glass, the critical internal angle is 42°

For water, it is 49°

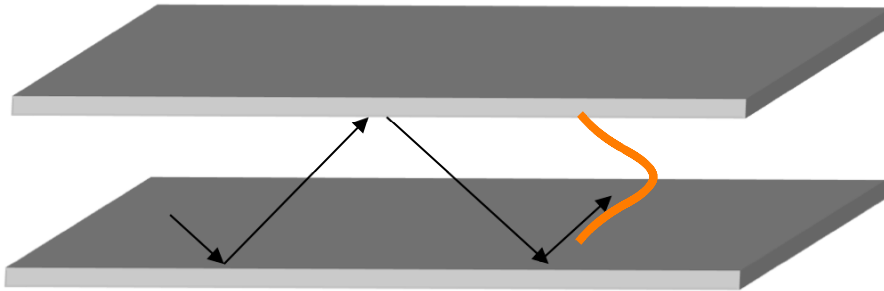


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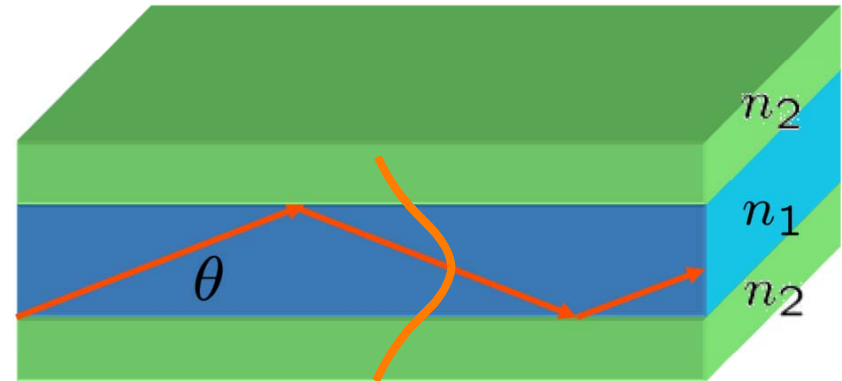


Waveguide Transport Light Between Mirrors

Metal waveguides



Dielectric waveguides



So what kind of waveguide are the optical fibers ?

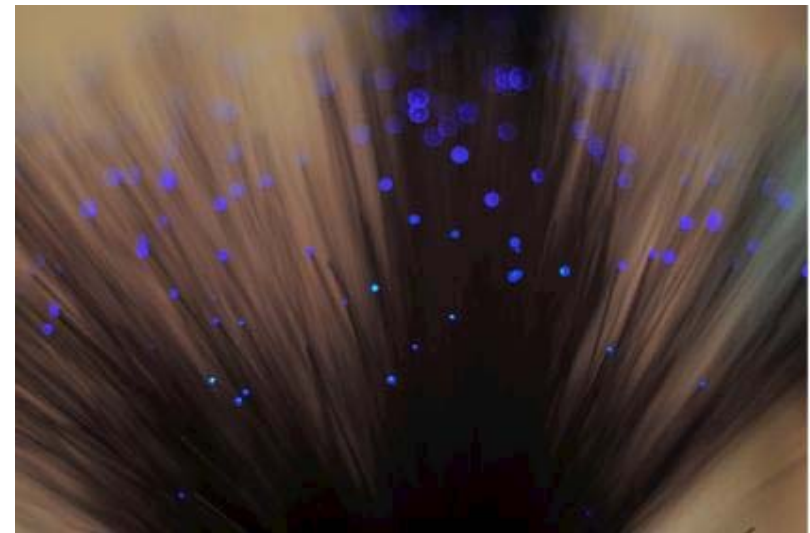


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Fabry-Perot Modes

Constructive Interference

$$r_{21} = \frac{n_2 - n_1}{n_2 + n_1}$$

$$E_r = rE_i$$

Standing Wave E-field

$$\lambda_{o1} = \frac{2n_1L}{m}$$

$$\lambda_{o2} = \frac{2n_2L}{m+1}$$

$$\Rightarrow \Delta\lambda_o = 2n_2L \left(\frac{1}{m} - \frac{1}{m+1} \right) = \frac{2n_2L}{m(m+1)}$$

$$\lambda_o = 1\mu m, \quad n_2 = 3.5, \quad L = 300\mu m$$

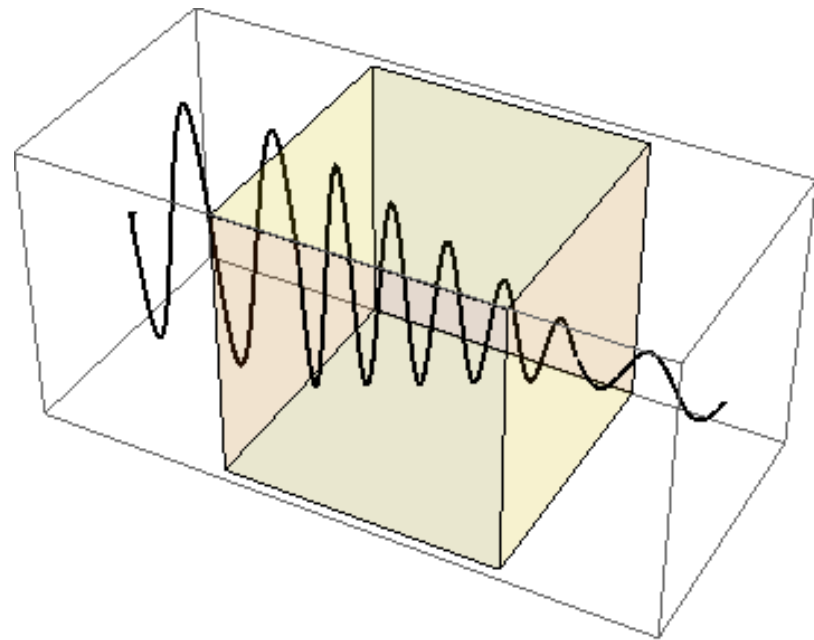
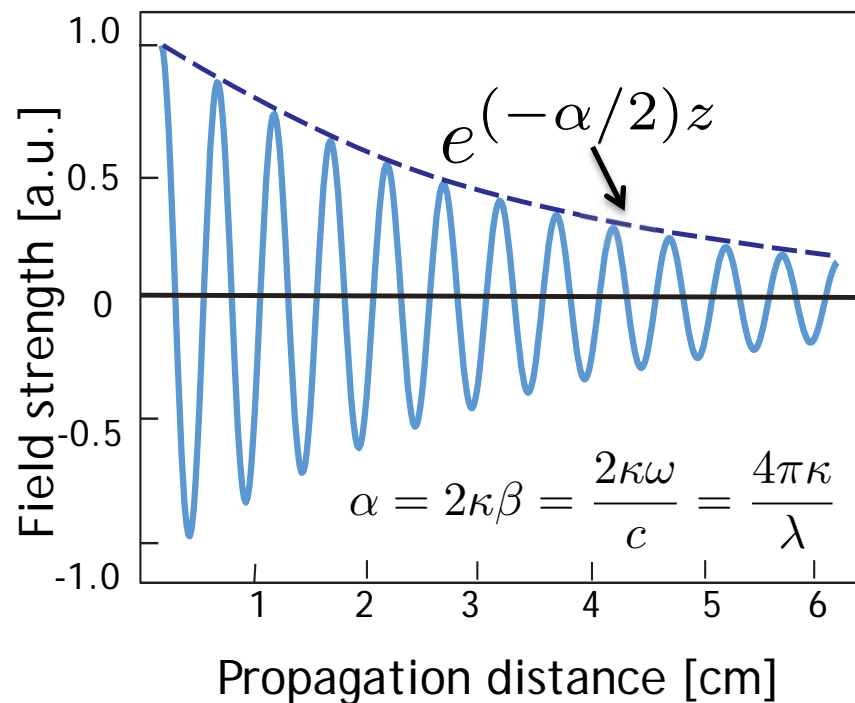
$$\lambda_1 = 1\mu m \Rightarrow m = 2100$$

$$\Delta\lambda = 5\text{\AA}$$

Plane Waves in Lossy Materials

$$E_y = \text{Re}\{A_1 e^{j(\omega t \tilde{k}z)}\} + \text{Re}\{A_2 e^{j(\omega t \tilde{k}z)}\}$$

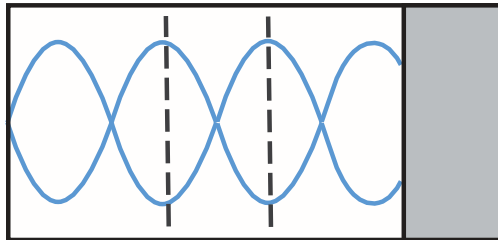
$$E_y(z, t) = A_1 e^{-\alpha/2z} \cos(\omega t - kz) + A_2 e^{+\alpha/2z} \cos(\omega t + kz)$$



Resonators with Internal Loss



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$$\tilde{r} = \frac{\tilde{n}_1 - \tilde{n}_2}{\tilde{n}_1 + \tilde{n}_2}$$

$$\tilde{t} = \frac{2\tilde{n}_1}{\tilde{n}_1 + \tilde{n}_2}$$

$$\frac{E_t}{E_i} = \frac{\tilde{t}_1 \tilde{t}_2 e^{-j\tilde{k}L}}{1 - \tilde{r}_1 \tilde{r}_2 e^{-2j\tilde{k}L}} = \frac{\tilde{t}_1 \tilde{t}_2 e^{-jk_r L} e^{-\alpha L}}{1 - \tilde{r}_1 \tilde{r}_2 e^{-2jk_r L} e^{-2\alpha L}}$$

...the EM wave loss is what heats the water inside the food

Laser Using Fabre-Perot Cavity

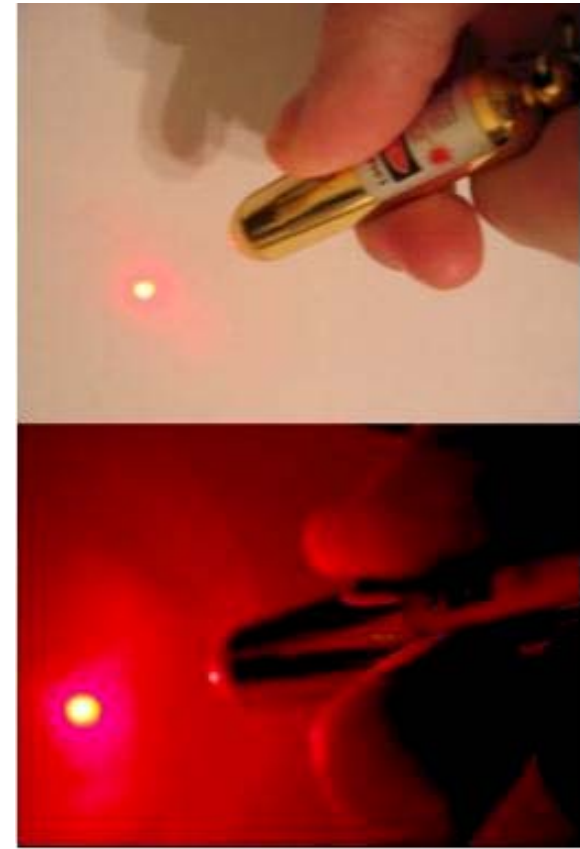
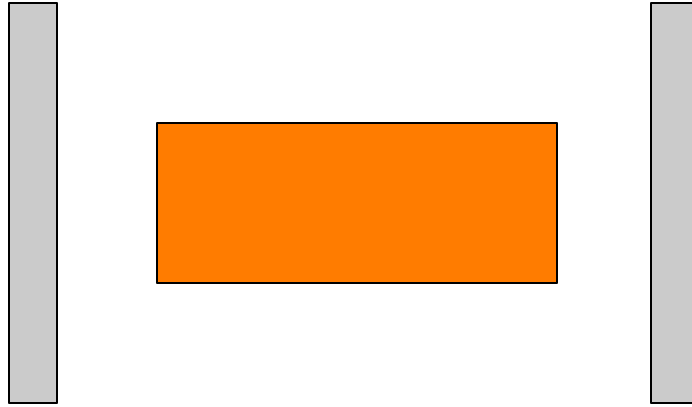
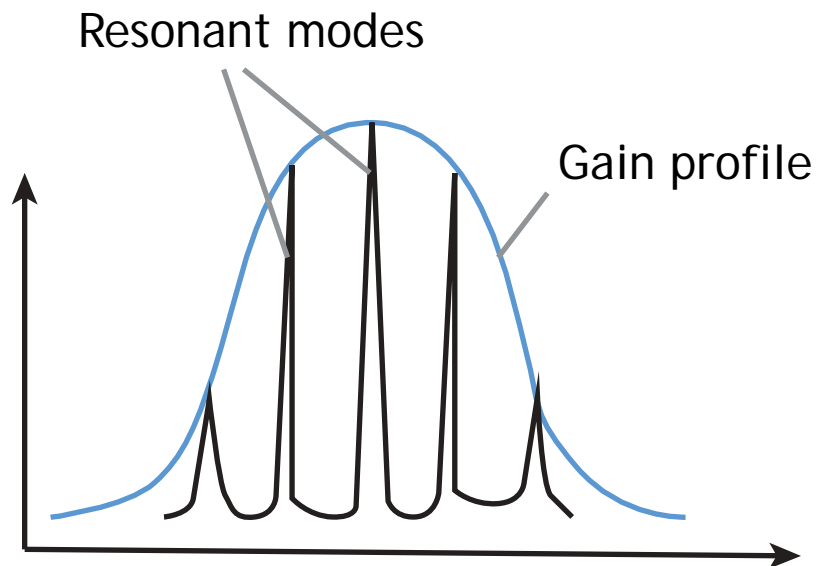
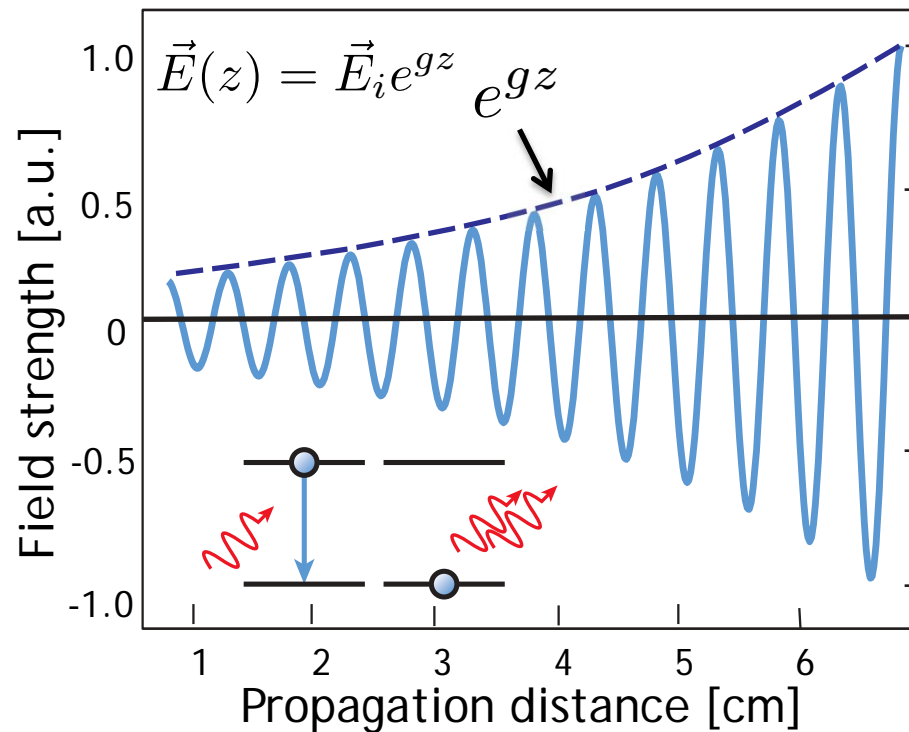


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Resonators with Internal Gain

What if it was possible to make a material with “negative absorption” so the field grew in magnitude as it passed through a material?



$$\frac{E_t}{E_i} = \frac{\tilde{t}_1 \tilde{t}_2 e^{-j\tilde{k}L}}{1 - \tilde{r}_1 \tilde{r}_2 e^{-2j\tilde{k}L}} = \frac{\tilde{t}_1 \tilde{t}_2 e^{-jk_r L} e^{-\alpha L}}{1 - \tilde{r}_1 \tilde{r}_2 e^{-2jk_r L} e^{-2\alpha L}}$$

Resonance:
 $e^{2jkL} = 1$

Lasers: Something for Nothing (almost)

at resonance $e^{2jkL} = 1$

$$\frac{E_t}{E_i} = \frac{\tilde{t}_1 \tilde{t}_2 e^{-j\tilde{k}L}}{1 - \tilde{r}_1 \tilde{r}_2 e^{-2j\tilde{k}L}} = \frac{\tilde{t}_1 \tilde{t}_2 e^{-jk_r L} e^{-\alpha L}}{1 - \tilde{r}_1 \tilde{r}_2 e^{-2jk_r L} e^{-2\alpha L}}$$

singularity at

$$1 = r_1 r_2 e^{\Gamma g L} e^{-\alpha_i L} \Leftrightarrow 1 = R_1 R_2 e^{2\Gamma g L} e^{-2\alpha_i L}$$

$$\frac{E_t}{E_i} \rightarrow \infty$$

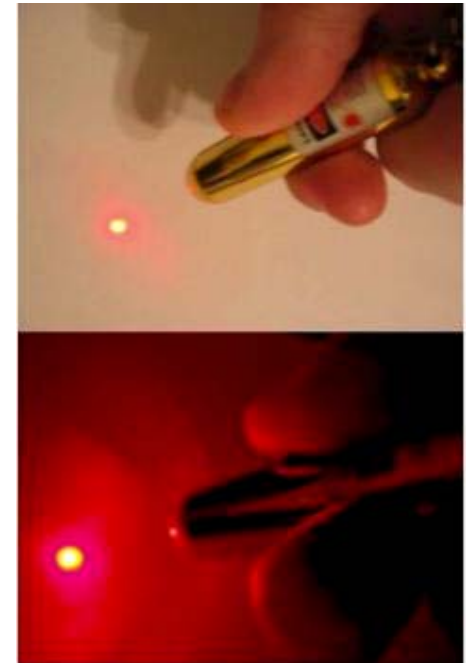


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