

**16.13 Aerodynamics of Viscous Fluids**  
**Problem Set 4**

Handed out: 3 Oct 01  
Due: 17 Oct 01

Write a program to solve the Falkner-Skan equation system by finite differences using the Newton-Raphson method. Attached is a program "template" with the matrix solver and input/output in place which will minimize pointless debugging. MATLAB or GNUPLOT are suggested for graphics. You can verify your solutions against the Falkner-Skan  $U(\eta)$  plots and parameter table handed out in class.

Your program is to have two basic modes: 1) Specified  $\beta_u$ , 2) Specified  $H$ .

1) Calculate a Falkner-Skan solutions for  $\beta_u = 1.0 \dots \beta_u =$  as low as possible ( $\simeq -0.09$ ). Using your computed profiles  $U(\eta; \beta_u)$ , compute and plot the resulting  $H(\beta_u)$  and compare with the  $H$  values from the class handout.

2) Calculate Falkner-Skan solutions for  $2.2 \geq H \geq 12$ , and plot  $H$  vs  $\beta_u$  again. Make sure you have enough points to adequately define this curve. Referring to this plot, explain the behavior of the Newton solution algorithm when a  $\beta_u$  value less than the minimum was specified in Question 1. Hint: It is a good idea to use the solution for one  $H$  as the starting guess for the next  $H$  value.

To suppress boundary layer separation, both suction ( $v_w < 0$ ) and a "moving wall" ( $u_w > 0$ ) have been tried experimentally. You are to examine the relative merits of each approach. Modify the boundary conditions and initial-guess profiles in the program to allow calculation of solutions with specified nonzero  $U_w = U(0)$  and nonzero  $V_w = V(0)$ . Note that you will have to define a transformed vertical velocity  $V$ , which is a similarity variable corresponding to  $v$ .

3a) With  $V_w = 0$ , determine the magnitude of  $U_w$  required to double the maximum sustainable adverse pressure gradient (minimum  $\beta_u \simeq -0.18$ ). Plot your result.

3b) With  $U_w = 0$ , determine the magnitude of  $V_w$  (negative) to achieve a minimum  $\beta_u \simeq -0.18$ . Plot your result.

3c) How practical would each approach be on an actual aircraft wing at  $Re_x = 10^6$ , say? Compare the physical  $u_w$  and  $v_w$  relative to  $u_e \sim$  flight speed.

Disclaimer: In reality the BL on an airfoil would be turbulent, but the comparison is valid on a relative basis.

In problem set 3, you calculated the drag of a thin airfoil, where the surface velocity was approximately described by a power law ( $u_e(x) \simeq u_\infty (x/c)^{\pm a}$ ). Boundary layer suction ( $u_w = 0, v_w < 0$ ) is now applied on the upper surface of the airfoil to suppress separation.

4a) Determine what, if any, restrictions must be placed on  $v_w(x)$  so that a similar boundary layer can still result.

4b) Using a value of  $\beta_u = -0.09$  and  $Re_c = 10^6$ , estimate the variation in profile drag of the airfoil as the magnitude of suction is increased. In reality, additional power is required to drive a suction system which would discharge the suction flow to freestream conditions. Assuming an ideal suction system, how should this additional power be included to provide a more meaningful estimate of the drag coefficient  $c_d$  of the airfoil? Is there an optimum suction flow that will result in a minimum overall  $c_d$ ?